Evaluation of Bio-Derived Synthetic Paraffinic Kerosenes (Bio-SPK)





Evaluation of Bio-Derived Synthetic Paraffinic Kerosenes

Approbation

We, representing parties who participated in the aviation biofuels testing described in this document, note by our signatures that we concur with the "Evaluation of Bio-Derived Synthetic Paraf nic Kerosenes" report.

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Evaluation of Bio-Derived Synthetic Paraffinic Kerosene (Bio-SPK)

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1.0 Introduction

It is of paramount importance that our industry must continue to progressively improve its environmental performance and lessen impacts to the global ecosystem, while continuing to reduce operating costs. Aviation recognizes these challenges must be addressed to ensure industry viability and is actively seeking to provide technologically driven solutions. Bio-derived jet fuel is a key element in the industry strategy to address these challenges. The signatories to this summary and many others have invested signi cant time and resources to further the research, development and commercialization of bio-derived jet fuel.

Virgin Atlantic paved the way with its proof of concept ight powered by biofuel in February 2008. Since that time, a broader range of fuels have become available that more closely replicate the performance characteristics of conventional kerosene jet fuel. Signi cant progress has been made in verifying the performance of Synthetic Paraf nic Kerosene (SPK) made from sustainable sources of bio-derived oils, that can be used in commercial aircraft at a blend ratio of up to 50 percent with traditional jet fuel (Jet A or Jet A-1). A cross-industry team consisting of Boeing, Honeywell/UOP, Air New Zealand (ANZ), Continental Airlines (CAL), Japan Airlines (JAL), General Electric, CFM, Pratt & Whitney, and Rolls-Royce participated in a series of tests ights with a bio-derived SPK (Bio-SPK) to collect data to support eventual certi cation of Bio-SPK jet fuels for use in commercial aviation pending the necessary approvals. This document provides a summary of the data collected from the Bio-SPK research and technology program, as well as a discussion about the additional data that is being generated to support fuel approval.

2.0 Fuel Development & Testing

2.1 Introduction

A sustainable alternative fuel can be described as one without negative environmental, economic, and

social impacts. In addition to having lower lifecycle green house gas (GHG) emissions, sustainable biofuels should not compete with food or fresh water resources or contribute to deforestation, while providing socioeconomic value to local communities where plant stocks are grown. Oil-based energy crops that can meet these sustainability criteria include, but are not limited to jatropha, camelina and algae. Based on the recent results of well-to-wake Life Cycle Assessments (LCA) carried out by Michigan Technological University in conjunction with UOP and Targeted Growth, Bio-SPK made from jatropha and camelina oils using the UOP renewable jet fuel process can achieve a reduction of GHG emissions between 65 and 80 percent relative to petroleumderived jet fuel. Similar results are projected for algal oil-derived SPK pending commercialization of ef cient oil extraction techniques. These research efforts place aviation on a path to reduce environmental impacts relative to petroleum fuels, but the portfolio of ideal sustainable fuels that will support aviation in the future are still in the early stages of being identi ed.

A chemical processing technique was identi ed to convert these sustainable bio-derived oils (triglycerides and free fatty acids) to Bio-SPKs. First, the oils were cleaned to remove impurities using standard oil cleaning procedures. The oils were then converted to the shorter chain diesel-range paraf ns using UOP's Renewable Jet Process, which converts the natural oils by removing oxygen molecules from the oil and converting any ole ns to paraf ns by reaction with hydrogen. The removal of the oxygen atoms raises the heat of combustion of the fuel and the removal of the ole ns increases the thermal and oxidative stability of the fuel. A second reaction then isomerizes and cracks the diesel range paraf ns, to paraf ns with carbon numbers in the jet range. The end product is a Bio-SPK fuel that contains the same types of molecules that are typically found in conventional petroleum based jet fuel. A summary of the fuel production process and well-to-wake LCA is shown in Figure 2.1





Figure 2.1 UOP's Hydrotreated Renewable Jet Process and LCA

2.2 Fischer-Tropsch SPKs (FT-SPKs) and Bio-SPKs

There has been extensive evaluation of SPK produced from a starting material using the Fischer-Tropsch process. A leader in developing and commercializing this technology is Sasol located in Johannesburg, South Africa, and the Sasol FT-SPK jet fuel is approved for use in commercial aviation, but not broadly available. There are many similarities between the processes and the nal SPK fuel using a starting material produced by the Fischer-Tropsch process and a process that uses a bio-derived oil. In both processes the nal steps is hydroprocessing followed by separation.

2.3 Bio-SPK Fuel Composition and Performance Data

2.3.1 Hydrocarbon Composition of Bio-SPK Fuel Samples

The hydrocarbon composition of the Bio-SPK fuels produced for the test ights were examined by advanced analytical techniques GC-MS, GCxGC-MS and CHN analysis. The result of the analysis was that the Bio-SPK fuels were composed of a combination of normal and iso-paraf ns with a small percentage of cyclo-paraf ns. The paraf ns carbon number and type (iso and n) of the neat Bio-SPKs varies from C9 to C15 which is a typical range found in conventional jet fuel; see Figure 2.2.



Figure 2.2 Carbon number and type (iso and n) distribution of neat Bio-SPK samples

D5291	Camelina SPK	Jatropha SPK	Jatropha-Algae SPK	Camelina- Jatropha-Algae SPK
% C	85.4	85.4	85.7	85
%Н	15.1	15.5	15.1	15
% N	< 0.10	< 0.10	< 0.10	<0.10
% C+% H	100.5	100.9	100.8	100
C/H	5.7	5.5	5.7	5.7

Table 2.1 shows the CHN elemental analysis of the Bio-SPK samples by D5291. The samples arepure hydrocarbons with a high level of saturation.

2.3.2 Trace materials

The Bio-SPK samples were further examined for low levels of impurities that could affect the performance of the fuel. The Bio-SPK samples were screened for sulfur, nitrogen and oxygen compounds in addition to 21 metals. The results of the analysis demonstrated that the Bio-SPK jet fuels did not contain any traceable amount of impurities as shown in Table 2.2. It can also be seen that the neat Bio-SPKs are virtually sulfur-free.

2.3.3 Additional Tests

Additional tests have been performed to fully characterize the Bio-SPKs in order to facilitate their approval.

- The dielectric constant of the Bio-SPKs was measured over the temperature range 40°C to +60°C. There is no requirement per ASTM D1655 to measure the dielectric constant of the jet fuel; however, it is very important to the fuel quantity indication system (FQIS).
- The density of each sample and their temperature dependence was measured per ASTM D4052 test method.

			ANZ	CAL	JAL	
Property		Specification	Jatropha	Jatropha/Algae	Camelina/ Jatropha/Algae	ASTM test
NON-HYDROCARBON COMPOSITION						
Oxygen, wt %			< 0.03	< 0.03	< 0.03	UOP
Nitrogen, ppm		2	<0.4	<0.4	<1	D4629
Water, ppm		75	32.0	34.0	19.0	D6304
Sulfur, ppm		15	< 0.01	<0.01	<0.01	D5453
Sulfur, mass %		0.0015	< 0.0001	< 0.0001	0.0001	D2622
Metals, ppm	Max	0.1 per metal				
Al, Ca, Co, Cr, Cu, Fe, K, Mg, Mn, Mo, Na, Ni, P, Pb, Pd, Pt, Sn, Sr, Ti, V, Zn			<0.1ppm	<0.1ppm	<0.1ppm	
Halogens, ppm	Max	1	<0.1	<0.1	0.2	D7359

Table 2.2 Chemical analysis of neat Bio-SPKs compared to requirements ofTable A1-2 from Dxxxx

- A materials compatibility study has been performed with neat Bio-SPKs to check the integrity of aircraft parts in contact with the Bio-SPK fuel; this is important for aspects such as seal swell needed in certain ttings. All samples passed compatibility requirements.
- The boiling point distribution was measured on all Bio-SPK jet fuels and the results show that there is a continuous distribution of hydrocarbons in these samples.

The thermal stability of the Bio-SPKs was checked by JFTOT (ASTM D3241) test method. The "breakpoint" is the highest control temperature at which the fuel meets tube rating and DP speci cation requirements. All of the neat Bio-SPKs have been tested at 340°C and passed the test as shown in Table 2.3.

$ \begin{array}{c c c c c c } \hline \begin{tabular}{ c c c c } \hline Partial Part$					ANZ		CAL	JAL	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Property		Jet A/Jet A-1	JP-8	Jatropha	Camelina	Jatropha/Algae	Camelina/Jatropha/Algae	ASTM Test Method
Acidly, total mg KOH/g Max 0.10 0.01 0.002 0.001 0.003 0.003 D3222 1. Aromatics, volume % Max 25 25 0.0 0.3 0.0 D319 2. Aromatics, volume % Max 0.03 0.001 <0.0001	COMPOSITION								
$\begin{array}{c c c c c c c } \hline A condition of the section of$	Acidity, total mg KOH/g	Max	0.10	0.015	0.002	0.002	0.001	0.003	D3242
1. Aronatics, volume % Max 25 25 0.0 0.3 0.0 Di19 Do57 Sulfar, metaplar, mas % Max 0.03 0.0001 <0.0001	Aromatics								
2. Aromatics, vol ume% Max 26.5 5	1. Aromatics, volume %	Max	25	25	0.0	0.3	0.0		D1319
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Aromatics, vol ume%	Max	26.5						D6379
Sulfar, mercapian, mass % Max 0.003 0.0001 < 0.0001 < 0.0001 < 0.0001 < 0.0001 D227 Sulfar, rotal mass % Max 0.30 0.30 < 0.0001 < 0.0001 0.0001 D2060, D262, D4294 or D5453 VolATLHTY D2887 or D86 D2887 or D86 Distillation requirements shall be met: D2887 or D86 D2887 or D86 Distillation requirements shall be met: report 168-229 168 162 164 163 So % recovered, temperature (T90) report 183-262 227 226 233 226.3 Distillation residue, % Max 1.5 1.5 1.3 1.2 1.2 Distillation residue, % Max 1.5 1.0 0.2 0.3 0.3 Distillation residue, % Max 3.4 0.75.5 0.75.8 0.75.8 0.75.8 0.75.8 0.75.8 0.75.8 0.75.8 0.75.8 0.75.8 0.75.8 0.75.8 0.75.8 0.75.8 0.75.8 0.75.8 0.75.9 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>									
Sulfar, total mass % Max 0.30 0.30 <0.0001 <0.0001 0.0001 D1266, D2622, D4294 or D5453 Vol.ATILITY Distillation: tome of the following requirements shall be met: D2887 or D86 Doe of the following requirements shall be met: D2887 or D86 D'6 recovered, temperature (T10) Max 205 157-205 168 162 164 163 90 % recovered, temperature (T00) report 1683-202 218 186 187 183 09 % recovered, temperature (100) Max 1.5 1.5 0.1 0.2 0.3 0.3 Distillation rescue, % Max 1.5 1.5 0.1 0.2 0.3 0.3 Distillation rescue, % Max 1.5 1.5 0.1 0.2 0.3 0.3 Distillation rescue, % Max 1.5 1.5 0.1 0.2 0.3 0.3 Distillation rescue, % Max 1.5 0.75 0.75 <	Sulfur, mercaptan, mass %	Max	0.003	0.002	0.0001	< 0.0001	< 0.0001	< 0.0001	D3227
VOLTUTY One of the following requirements shall be met: D2887 or D86 Distillation is point reportante, C: Image: C: </td <td>Sulfur, total mass %</td> <td>Max</td> <td>0.30</td> <td>0.30</td> <td>< 0.0001</td> <td>< 0.0001</td> <td>< 0.0001</td> <td>0.0001</td> <td>D1266, D2622, D4294 or D5453</td>	Sulfur, total mass %	Max	0.30	0.30	< 0.0001	< 0.0001	< 0.0001	0.0001	D1266, D2622, D4294 or D5453
Distillation: One of the following requirements shall be me: D288 or D86 Distillation renperature; °C: 10 % recovered, temperature (T10) Max 205 157-205 168 162 164 163 90 % recovered, temperature (T10) Max 205 157-205 168 122 228 226 233 226.33 226.33 90 % recovered, temperature (T00) report 168.229 18 18.6 187 183. 226.33 236.33 236.30 236.30 236.30 236.30 336.35.10 <t< td=""><td>VOLATILITY</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	VOLATILITY								
One of the following requirements shall be met: J288' or D86 10% recovered, temperature (T10) Max 205 157-205 168 162 164 163 10% recovered, temperature (T50) report 183-262 227 226 233 226.3 90% recovered, temperature (T90) report 183-262 227 226 233 226.3 Distillation residue, % Max 1.5 1.3 1.3 1.2 1.2 Distillation residue, % Max 1.5 1.3 0.1 0.2 0.3 0.3 Final bolting point, temperature (simul) Max 340 - - - - - Eash point, *C 0.775-0.840 0.775 0.749 0.753 0.748 0.752 D1298 or D4052 Fuezing point, *C Max -47 Jet A-1 -47 -57.0 -63.5 -54.5 -63.5 D972, D7153, D7154 or D2386 Viscosity -20°C, mm ² /s Max -47 Jet A-1 -47 -57.0 -63.5 -54.5 -63.5 D972, D7153, D7154 or D2386 OMBUSTON 13.4 1.4	Distillation:								
Distillation temperature, "C: 10% recovered, temperature (T00) 10% recovered, temperature (T00) report 168-229 168 166 168 162 168 162 168 162 168 162 168 162 168 162 168 162 168 162 163 163 163 163 163 163 163 163	One of the following requirements shall be met:								D2887 or D86
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Distillation temperature, °C:		205	167.005	1(0	1/2	1/1	10	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	10 % recovered, temperature (110)	Max	205	157-205	168	162	164	163	
90 % recovered, temperature (190) Teport Tis3>202 227 226 233 226.3 Final boiling point, temperature (190) Max 1.5 1.5 1.3 1.3 1.2 1.2 Distillation oss, % Max 1.5 1.5 0.1 0.2 0.3 0.3 Final boiling point, temperature (simul) Max 340 - 0.3 0.3 Plash point, % Max 340 - 0.75 0.3 0.3 Density at 15°C, kg/L 0.775-0.840 0.75 0.749 0.733 0.748 0.752 D1298 or D4052 FLIDITY - 0.775-0.840 0.840 -	50 % recovered, temperature (150)		report	168-229	188	186	18/	183	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	90 % recovered, temperature (190)	Man	report	183-262	227	226	233	226.3	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Pinal bolling point, temperature	Max	300	300	255	251	250	237.7	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Distillation loss %	Max	1.5	1.5	1.5	1.5	1.2	1.2	
$\begin{array}{c c c c c c } \label{eq:construction} \begin{tikzed}{line}{lin$	Einal hailing point tamparatura (aimul)	Max	1.5	1.5	0.1	0.2	0.5	0.3	
I has point, CMinJobJobJobJobJobJobJobJobJobDensity at ISC, kg/L0.775-0.840 $0.775-0.840$ 0.749 0.733 0.748 0.752 D1298 or D4052FLUIDITYFreezing point, °CMax -40 Jet A -47 Jet A-1 47 -57.0 -63.5 -54.5 -63.5 -54.5 -63.5 D5972, D7153, D7154 or D2386Viscosity -20°C, nm²/sMax8.08.03.6633.336 3.510 3.353 D445COMBUSTIONNet heat of combustion, MJ/kgMin 42.8 42.8 44.3 44.0 44.2 44.2 44.2 4529 , D3338 or D4809One of the following requirements shall be met:(1) Smoke point, mn, orMin 18 19 Naphthalenes, volume, %Max 3.0 3.0 <0.01 <0.01 <0.01 <0.01 <122 (D1302CORRENTORCorrestore, manyMin 18 19 Na >0.01 <0.01 <0.01 <0.01 <0.01 <0.01 <0.01 >0.01 <td< td=""><td>Flash point °C</td><td>Min</td><td>28</td><td>28.68</td><td>16.5</td><td>42.0</td><td>41.0</td><td>42.0</td><td>D56 or D2828</td></td<>	Flash point °C	Min	28	28.68	16.5	42.0	41.0	42.0	D56 or D2828
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	r iasii point, 'e	with	50	0.775-	40.5	42.0	41.0	42.0	D50 01 D5020
FLUIDITY Server and the	Density at 15°C, kg/L		0.775-0.840	0.840	0.749	0.753	0.748	0.752	D1298 or D4052
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	FLUIDITY			0.010					
Freezing point, *C Max Max 47 47 -57.0 -63.5 -54.5 -63.5 D5972, D7153, D7154 or D2386 Viscosity -20°C, mm ² /s Max 8.0 8.0 8.0 3.363 3.310 3.353 D445 COMBUSTION Net heat of combustion, MJ/kg Min 42.8 42.8 44.3 44.0 44.2 44.2 D4529, D3338 or D4809 Hydrogen content, mass % Min 13.4 1 D1322 D134 D134 D134 D134 D1322 D134 D			-40 Jet A						
Viscosity -20°C, mm ² /s Max No.1 8.0 3.663 3.336 3.510 3.353 D445 COMBUSTION No.1 8.0 3.663 3.364 3.510 3.353 D445 Net heat of combustion, MJ/kg Min 42.8 44.3 44.0 44.2 44.2 D4529, D3338 or D4809 Hydrogen content, mass % Min 13.4 13.4 13.4 1000<	Freezing point, °C	Max	-47 Iet A-1	-47	-57.0	-63.5	-54.5	-63.5	D5972, D7153, D7154 or D2386
COMBUSTIONInternational and the stateInternational and the stateInternational and the stateInternational and the stateInternational and the stateNet heat of combustion, MJ/kgMin42.842.844.344.044.244.244.2Public groutements shall be met:International and the stateInternational and the stateInternational and the stateInternational and the state(1) Smoke point, mm, orMin1819International and the stateInternational and the state(2) Smoke point, mm, andMin1819International and the stateInternational and the state(2) Smoke point, mm, andMin1819International and the stateInternational and the state(2) Smoke point, mm, andMin1819International and the stateInternational and the state(2) Smoke point, mm, andMin1819International and the stateInternational and the state(3) Smoke point, mm, andMin1819International and the stateInternational and the state(3) Smoke point, mm, andMin1819International and the stateInternational and the state(3) Smoke point, mm, andMin1819International and the stateInternational and the state(3) Smoke point, mm, and the stateNo.1No.1No.1No.1International and the state(4) StateAdditional and the stateAdditional and the stateInternational and the stateInternational and the state <td>Viscosity -20°C mm²/s</td> <td>Max</td> <td>8.0</td> <td>8.0</td> <td>3 663</td> <td>3 336</td> <td>3 510</td> <td>3 353</td> <td>D445</td>	Viscosity -20°C mm ² /s	Max	8.0	8.0	3 663	3 336	3 510	3 353	D445
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	COMBUSTION	mun	0.0						5115
Hydrogen content, mass %Min13.4International of the following requirements shall be met:(1) Smoke point, mm, orMin2525D1322(2) Smoke point, mm, andMin1819D1322Naphthalenes, volume, %Max3.0 <0.01 <0.01 <0.01 <0.01 CORROSIONCORROSIONTHERMAL STABILITYD130FTOT (2.5 h at control temperature)T <340 340 340 300 03241 FTOT (2.5 h at control temperature)Tube deposits less than 3 3 1 <1 1 CONTAMINANTS 33 3 1 <1 1 1	Net heat of combustion MI/kg	Min	42.8	42.8	44 3	44.0	44.2	44.2	D4529 D3338 or D4809
	Hydrogen content, mass %	Min		13.4					,
	One of the following requirements shall be met:								
(2) Smoke point, mm, and Min 18 19 D1322 Naphthalenes, volume, % Max 3.0 3.0 <0.01	(1) Smoke point, mm, or	Min	25	25					D1322
Naphthalenes, volume, % Max 3.0 3.0 <0.01 <0.01 <0.01 <0.01 <0.01 D1840 CORROSION No.0 No.1 No.1 No.1 No.1 D130 THERMAL STABILITY JF107 (2.5 h at control temperature) J J D130 Temperature, °C Min 260 340 340 340 300 D3241 Filter pressure drop, mm Hg Max 25 25 Tube deposits less than 3 3 1 <1 1	(2) Smoke point, mm, and	Min	18	19					D1322
CORROSION Copper strip, 2 h at 100°C Max No. 1 No. 1 No. 1 Diamontana THERMAL STABILITY JFTOT (2.5 h at control temperature) JFTOT (2.5 h at control temperature, °C Min 260 340 340 300 D3241 Temperature, °C Max 25 25 Tube deposits less than 3 3 1 1	Naphthalenes, volume, %	Max	3.0	3.0	< 0.01	< 0.01	< 0.01	< 0.01	D1840
Copper strip, 2 h at 100°C Max No. 1 No. 1 No. 1 D130 THERMAL STABILITY D130 JFOT (2.5 h at control temperature) 340 340 340 300 D3241 Temperature, °C Max 25 25 3 3 1 Tobe deposits less than 3 3 1 1 1	CORROSION								
THERMAL STABILITY JFTOT (2.5 h at control temperature) JFTOT (2.5 h at control temperature) Temperature, °C Min 260 340 340 300 D3241 Filter pressure drop, mm Hg Max 25 25 Tube deposits less than 3 3 1 CONTAMURANTS 1 1 1	Copper strip, 2 h at 100°C	Max	No. 1	No. 1					D130
JFTOT (2.5 h at control temperature) JETOT (2.5 h at control temperature, °C Min 260 340 340 300 D3241 Temperature, °C Min 260 25 0 <t< td=""><td>THERMAL STABILITY</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	THERMAL STABILITY								
Temperature, °C Min 260 340 340 340 300 D3241 Filter pressure drop, mm Hg Max 25 25 1	JFTOT (2.5 h at control temperature)								
Filter pressure drop, mm Hg Max 25 25 Tube deposits less than 3 3 1 CONTAMURANTS	Temperature, °C	Min	260		340	340	340	300	D3241
Tube deposits less than 3 3 1 <1 1	Filter pressure drop, mm Hg	Max	25	25					
CONTAMINANTS	Tube deposits less than		3	3	1	<1	1	1	
CONTRADUCTO	CONTAMINANTS		_	_					
Existent gum, mg/100 mL Max 7 7 7 <1 <1 <1 D381, IP 540	Existent gum, mg/100 mL	Max	7	7		<1	<1	<1	D381, IP 540

Table 2.3 Properties summary of neat Bio-SPKs against existing jet fuel speci cations

2.4 Bio-SPK Flight Test Program Samples

After an initial screening of the Bio-SPKs, a decision was made to conduct a series of ight tests using a 50 percent by volume blend of Bio-SPK and petroleumbased jet fuel. As part of the test program, laboratory fuel property testing took place at multiple locations including Boeing, Honeywell/UOP, Air Force Research Lab (AFRL), several independent outside laboratories and at participating engine companies. The three Bio-SPK fuels used for the ights and the CFM engine ground test effectively met all ASTM D1655 performance speci cations at a 50 percent blend with petroleum-based jet fuel (Table 2.5). Additional property and performance tests were performed to support approval to use the experimental fuels including materials compatibility testing. A summary of the test ights and the feedstocks that were used to produce the fuel are shown in Table 2.4 below: In all of the Bio-SPK test ights only one engine was fed with the Bio-SPK jet fuel blend.

Airline	Air New Zealand	Continental Airlines	Japan Airlines	
Aircraft	Boeing 747-400	Boeing 737-800	Boeing 747-300	
Engine	Rolls-Royce RB211-524G	CFM International CFM56-7B	Pratt & Whitney JT9D-7R4G2	
Plant Feedstock	50% jatropha	47.5% jatropha, 2.5% algae	42% camelina, 8% jatropha/algae	
Fuel Provider for Test Flight	UOP	UOP	Nikki Universal/UOP	
Flight date	Dec 30, 2008	Jan 7, 2009	Jan 30, 2009	
Engine Tests/Ground Run Results	Comparison of fuel flow with expected heat of combustion	Engine Operability & Emissions Tests for various blend percentages	Engine Operability & Emissions on Neste Oil-provided paraffins for ground engine test only.	
Flight Test Profile	Climb to FL 350, Mach 0.84 accels & decels, engine windmill restarts, starter-assisted engine relights, simulated missed approach, suction feed test	Climb to FL390, Mach 0.78, accels & decels, engine windmill restarts, starter- assisted engine relights, simulated missed approach, suction feed test	Climb to FL390, Mach 0.80, accels & decels, engine windmill restart, suction feed test. Was the only hydro-mechanical engine used for this series of flight tests.	

Table 2.4 Bio-SPK Test Flight Summary

Property		Jet A / Jet A-1	ANZ	CAL	JAL	ASTM Test Method	
Mixture of Jet A or Jet A-1 // SPK is in			50	50	50		
Volume % Blended with			Jet A-1	Jet A	Jet A		
Part 1: Basic Requirements							
COMPOSITION		0.10	0.000	0.001	0.000	D2242	
Acidity, total mg KOH/g	Max	0.10	0.002	0.001	0.002	D3242	
he met							
1. Aromatics, volume %	Max	25	8.8	9.2	8.9	D1319	
2. Aromatics, volume %	Max	26.5	N/A	N/A	N/A	D6379	
Sulfur mercantan ^C mass %	Max	0.003	0.0004	<0.0001	0.0003	D3227	
Sulfur, increaptan, indiss // Sulfur, total mass %	Max	0.30	< 0.015	< 0.0001	0.0403	D1266, D2622, D4294 or D5453	
VOLATILITY						, ,	
Distillation:						Danas Dar	
Distillation temperature, °C:	Ман	205	170.4	170.5	171.0	D2887 or D86	
50 % recovered, temperature (T50)	wax	203 report	1/0.4	170.5	200.5		
90 % recovered, temperature (T90)		report	226.9	228.0	200.5		
Final boiling point, temperature	Max	300	246.8	248.5	258.0		
Distillation residue, %	Max	1.5	1.2	1.2	1.2		
Distillation loss, %	Max	1.5	0.4	0.2	0.2		
Flash point, °C	Min	38	45.0	45.0	44.5	D56 or D3828	
Density at 15°C, kg/m ³		775 to 840	779	780	789	D1298 or D4052	
FLUIDITY							
Freezing point, °C	Max	-40 Jet A	-62.5	-61.0	-55.5	D5972, D7153, D7154 or D2386	
		-47 Jet A-1	2.000	2.017	4 205	D445	
Viscosity –20°C, mm ² /s	Max	8.0	3.606	3.817	4.305	D445	
COMBUSTION Net heat of combustion MI/kg	Min	128	13.6	13.7	13.5	D4529 D2228 or D4809	
One of the following requirements shall be met:	IVIIII	42.0	43.0	43.7	43.5	D4529, D5558 01 D4809	
(1) Smoke point mm or	Min	25	33			D1322	
(2) Smoke point, mm, and	Min	18	55	27.7	28.6	D1322	
Naphthalenes, volume, %	Max	3.0	N/A	0.2	1.2	D1840	
CORROSION							
Copper strip, 2 h at 100°C	Max	No. 1	1A	1A	1A	D130	
THERMAL STABILITY							
JFTOT (2.5 h at control temperature)	M	2(0	200	200	200	D2241	
Filter pressure drop, mm Ha	Min	260	300	300	300	D3241	
Tube deposits less than	IVIAX	2.5	1.0	1.0	1.0		
rube deposits less than	No	Peacock or Abno	rmal Color De	eposits	1.0		
CONTAMINANTS				r · · ·			
Existent gum, mg/100 mL	Max	7	1.0	<1	<1	D381, IP 540	
Microseparometer, Rating						D3948	
Without electrical conductivity additive	Min	85					
With electrical conductivity additive	Min	70					
ADDITIVES		See 6.3	122.0	-1	-1	D2(24	
Electrical conductivity, pS/m		Dant 2. Extanda	123.0 1 Dequinement	<1 •**	<1	D2624	
COMPOSITION							
Aromatics: one of the following requirements shall							
be met							
1. Aromatics, volume %	Min	8	8.8	9.2	8.9	D1319	
2. Aromatics, volume %	Min	8.4	N/A	N/A	N/A	D6379	
Distillation						D2997 or D96	
Distillation:	Min	15	10.0	22.5	20.5	D288/ 01 D80	
T90-T10, C.	Min	40	56.5	23.5 57.5	69		
170 110, 0.		70	50.5	57.5	07		
Lubricity, mm	Max	0.85	0.64	0.65	0.66	D5001	

2.5 Properties summary for the Bio-SPK jet fuel blends

Table 2.5 Comparison with data from Table 1 from Dxxxx, Detailed Requirements of AviationTurbine Fuels Containing Synthesized Hydrocarbons

3.0 Engine Operability, Emissions, & Flight Test Program

Engine tests occurred at General Electric's Ohio facility on a fully instrumented CFM56-7B development engine. Performance and operability testing in addition to emission evaluation were performed comparing a baseline Jet A with 50 percent and 25 percent Bio-SPK fuel blends, respectively. Performance testing measured Speci c Fuel Consumption (SFC) at several power settings from ground idle to take-off. Operability testing measured start times, lean-blow out margin, acceleration and deceleration times. The emissions testing measured the currently regulated emissions species; Nitrogen Oxides (NOx), Carbon Monoxide (CO), hydrocarbons (HC), and smoke number. The emissions of the Bio-SPK fuel blends all measured within the normal expected variation of jet fuel.

A series of engine ground runs were conducted on an Air New Zealand Boeing 747-400 aircraft equipped with Rolls Royce RB 211-524G engines prior to the test ight including a switch of fuel at various progressions of Engine Pressure Ratio (EPR) settings. The engine showed no change in behavior from an operational perspective. The Digital Flight Data Recorder (DFDR) data from the EPR of 1.4 is shown in Figure 3.1. The 1.07 percent lower fuel ow that was observed on the engine run of the Bio-SPK jet fuel blend is consistent with the 1.08 percent higher energy density per unit mass of the Bio-SPK fuel blend, which was determined experimentally.

For all ights, a detailed analysis was made for the following parameters from each engine, as applicable, for parameters such as altitude, airspeed (VCAS), engine pressure ratio, N1%, N2%, N3%, EGT (C°), P3, fuel ow, and throttle angle. Also, borescope analyses were conducted before and after each test to detect any potential engine deterioration.



Figure 3.1 Engine ground run data is shown from a Rolls Royce RB211-524G engine taken at Auckland on Dec. 30 2008. The data shows a reduction in fuel ow, due to the higher heat of combustion of the 50 percent Bio-SPK fuel blend.

4.0 Performance Summary

Findings from this research and test program, as well additional testing that is currently in progress, will be used to support sustainable biofuel development and approval for use in aviation. The program engaged fuel suppliers, engine companies, and the airlines as a team effort to address industry concerns about CO₂ emissions, fuel availability, and cost. A commercial-ready Bio-SPK fuel production process was scaled upward from the initial DARPA program research phase, to demonstrate its viability to produce a replacement jet fuel blend and fuel property that takes airframe compatibility and engine operability & emissions tests into consideration. The Bio-SPK fuel blends used in the test ights have all either met or exceeded the performance speci cations for jet fuel. For example, the Bio-SPK fuel blends demonstrated higher energy density per unit mass than typical jet fuel, enabling airplanes to travel farther using less fuel. For all of the test ights, the blended biofuel displayed no adverse effects on any of the aircraft systems.

5.0 Next Steps – Fuel Approval

The Bio-SPK ight test and research program generated valuable data to support approval of Bio-SPK at up to a 50 percent blend ratio. Boeing, in cooperation with Honeywell/UOP and the US Air Force Research Laboratory, is currently preparing a comprehensive research report to be submitted to the ASTM International Aviation Fuel Committee, which will follow the guideline outlined in the revised ASTM D4054 document entitled "Standard Practice for Quali cation and Approval of New Aviation Turbine Fuels and Fuel Additives." Reporting for other fuel speci cations will be made, as required. The majority of t-for-purpose and auxiliary power unit engine and combustion rig tests have been completed in addition to emission evaluation. We are currently gathering data from these tests for inclusion in the research report along with data generated from the Bio-SPK ight test program. Preliminary examination of the results of those tests is extremely encouraging.

Glossary

Algae

Algae, which can be grown in brackish or polluted water, unsuitable for drinking or agriculture, can be harvested for oil which can be processed into biofuel. This isn't large scale yet, but could potentially provide a signi cant proportion of aviation's fuel needs.

ASTM International

Originally known as the American Society for Testing and Materials, this international standards organization develops and publishes voluntary consensus technical standards for a wide range of materials, services, systems and products.

Air Force Research Lab (AFRL)

Headquartered at Wright-Patterson Air Force Base, Ohio, AFRL is a fullspectrum laboratory, responsible for planning and executing the US Air Force's science and technology program.

Biofuel

Fuel produced from renewable resources. Aviation is focused on advanced generation biofuels derived from sustainable biomass that do not impact the food supply chain or fresh water resources or contribute to deforestation.

Biomass

Any organic matter that can be converted into fuel.

Bio-SPK

A synthetic paraf nic kerosene that was produced from a bio-derived oil source

Neat Bio-SPK

100 percent Bio-SPK

DARPA

Defense Advanced Research Projects Agency

Fischer-Tropsch Process

A chemical reaction process that uses a catalyst to react carbon monoxide and hydrogen to make hydrocarbons.

Fischer-Tropsch SPK

A synthetic paraf nic kerosene that was produced from a starting material using the Fischer-Tropsch process

Free Fatty Acids

A carboxylic acid with an aliphatic chain that is either unsaturated or saturated in a mixture of triglyceride oil

Jet A/Jet A-1

Jet A is the recognized US speci cation for jet fuel, Jet A-1 is the internationally recognized speci cation for jet fuel outside of North America. Both speci cations have similar criteria for density, heating values (i.e. energy contents), but Jet-A1 has a slightly lower freeze point than Jet-A

Hydroprocessing

Hydroprocessing is process technology widely used in the renning industry for the production of clean, transportation fuels. The technology utilizes catalysts in the presence of hydrogen to convert a variety of feedstocks, including biologically derived materials, into high-quality fuels.

Iso-Paraf ns

Branched chain paraf ns

Jatropha

A plant that produces seeds which are an ef cient source of oil for conversion into Bio-SPK. It can be grown in arid regions on land that would not support food agriculture.

Kerosene

The common name for petroleum-derived jet fuel such as Jet A-1. In addition to its use in aviation, kerosene can be used for a variety of other purposes.

n-paraff ns

Straight chain paraf ns

Synthetic Paraf nic Kerosene (SPK)

Aviation fuel that contains predominantly paraf ns produced from nonpetroleum feedstocks

UOP

UOP LLC, a Honeywell company is a leading international supplier and licensor of process technology, catalyst, adsorbents, equipment and consulting services to petroleum re ning, petrochemical, and gas processing industries. UOP technology for the production of clean, high quality fuels and petrochemicals is used today in almost every re nery around the world.

UOP's Renewable Jet Process

Proprietary chemical processing techniques that can convert sustainable bio-derived oils (triglycerides and free fatty acids) to Bio-SPKs.

CHN

Carbon, Hydrogen, Nitrogen

GC-MS

Gas Chromatography-Mass Spectrometry. GC-MS is an analytical technique that combines gas chromatography with mass spectrometry to identify chemical compounds

GCxGC-MS

A gas chromatography method that utilizes two gas chromatography separation steps followed by analysis by mass spectrometry







